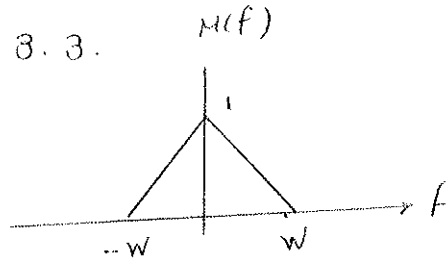


ECE 316 CHAPTER 3 PROBLEM SET SOLUTIONS

Drill. Problem 3.3.

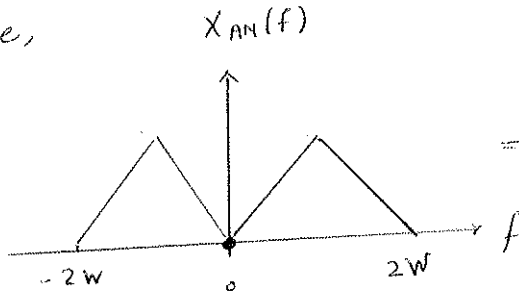
$$m(t) \xrightarrow{F} M(f)$$



$$x_{AM}(t) = A_c [1 + k_a m(t)] \cos 2\pi f_c t$$

⇒ Assume $f = W$

Therefore,



if $f > W$: No overlap

if $f = W$: spectral overlap

if $f < W$: overlap

2. Drill problem 3.1.

$$A_{min} = A_c (1 - \mu) = 0$$

100% modulation : $|k_a m(t)| = 1 \Rightarrow$ if $k_a m(t) = -1$

$A_c (1 + k_a m(t)) \cos \omega_c t = 0$ ⇒ envelope : $1 + k_a m(t) = 0$

3. Drill problem 3.2.

AM with a sinusoidal modulating signal :

$$s(t) = A_c (1 + k_a A_m \cos \omega_m t) \cos \omega_c t.$$

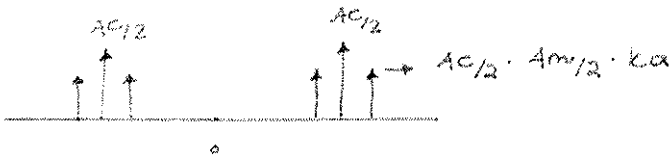
$$= A_c \cos \omega_c t + A_c \mu \cos \omega_m t \cos \omega_c t$$

$\mu = k_a A_m$ modulation factor.

Total average power components: $A_c^2/2$ (in carrier)

(upper-side freq) $2 \left(\frac{A_m^2}{4} \cdot \frac{A_c^2}{4} \cdot k_a^2 \right) = \frac{\mu^2 A_c^2}{8}$

(lower-side freq) $2 \left(\frac{A_m^2}{4} \cdot \frac{A_c^2}{4} \cdot k_a^2 \right) = \frac{\mu^2 A_c^2}{8}$



(a) Average power in the carrier: $A_c^2/2$.

(b) each side freq: $A_c^2/8 \cdot \mu^2 = (0.2)^2 A_c^2/8$ if $\mu = 0.2$.

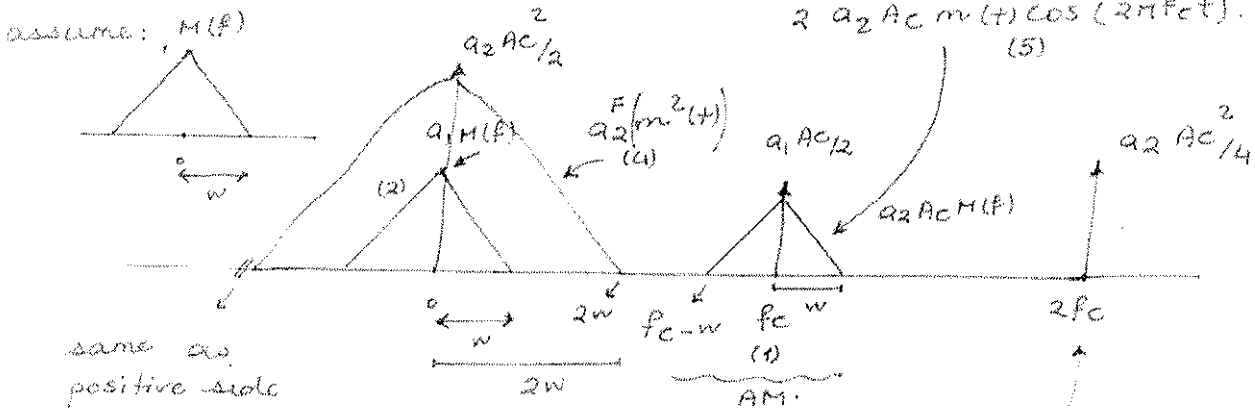
4. Drill problem 3.4. (* important).

$$v_1(t) = A_c \cos(2\pi f_c t) + m(t)$$

square law: $v_2(t) = a_1 v_1(t) + a_2 v_1^2(t)$

$$\Rightarrow v_2(t) = a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + a_2 [A_c \cos(2\pi f_c t) + m(t)]^2$$

$$= a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + a_2 A_c^2 \cos^2(2\pi f_c t) + a_2 m^2(t) + 2 a_2 A_c m(t) \cos(2\pi f_c t)$$



$$(3): a_2 A_c^2 \cos^2(2\pi f_c t) = a_2 A_c^2/2 [1 + \cos(4\pi f_c t)]$$

$$= a_2 A_c^2/2 + a_2 A_c^2/2 \cos(2(2\pi f_c t))$$

in summary:

$$(1) a_1 A_c \cos(2\pi f_c t) \xrightarrow{F} a_1 A_c / 2 \left[\delta(f - f_c) + \delta(f + f_c) \right]$$

$$(2) a_1 m(t) \xrightarrow{F} a_1 M(f) \quad (\text{baseband BW} = w)$$

$$(3) a_2 A_c^2 \cos^2(2\pi f_c t) = \underbrace{a_2 A_c^2 / 2}_{\substack{\downarrow \\ \text{DC signal} \\ (0 \text{ Hz})}} + \underbrace{a_2 A_c^2 / 2}_{\substack{\downarrow \\ F}} \cos(2(2\pi f_c t))$$
$$\xrightarrow{F} a_2 A_c^2 / 2 \delta(f) \quad a_2 A_c^2 / 4 \left[\delta(f - 2f_c) + \delta(f + 2f_c) \right]$$

$$(4) a_2 m^2(t) \xrightarrow{F} a_2 M(f) * M(f) \Rightarrow \text{BW} = 2w \quad (\text{baseband})$$

$$(5) 2 a_2 A_c m(t) \cos(2\pi f_c t) \xrightarrow{F} a_2 A_c \left[M(f - f_c) + M(f + f_c) \right]$$

(b) Combining (4) and (5)

$$a_1 A_c \cos(2\pi f_c t) + 2 a_2 A_c m(t) \cos(2\pi f_c t) =$$

$$a_1 A_c \left[1 + \frac{2 a_2}{a_1} m(t) \right] \cos(2\pi f_c t) \quad \text{AM signal.}$$

\Rightarrow BPF : f_c : centre frequency
 $\text{BW} = 2w.$

(c) To have no frequency distortion

$$f_c - w > 2w \Rightarrow \underline{\underline{f_c > 3w}}$$

($w < f_c < 2w$ mentioned in the book is INCORRECT).

Drill 3.6.

DSB - SC signal : $x_{DSB} = A_c m(t) \cos 2\pi f_c t$

where $m(t) = A_m \cos 2\pi f_m t$

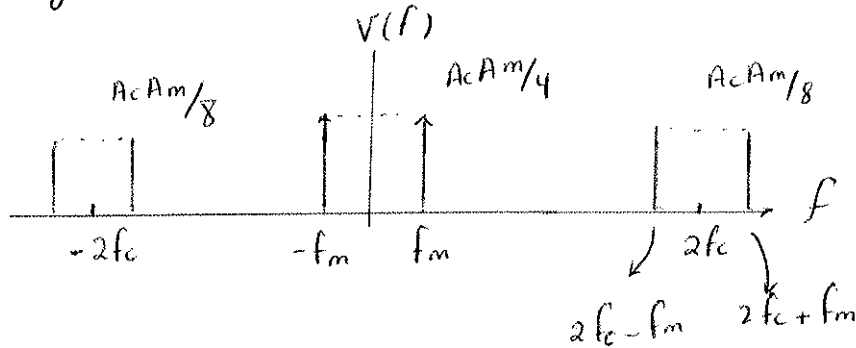
$\Rightarrow x_{DSB-SC} = A_c A_m \cos 2\pi f_c t \cos 2\pi f_m t$

Consider the received local oscillator as : $\cos 2\pi f_c t$

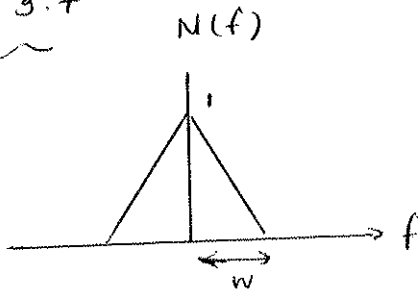
\Rightarrow The output $v(t) = A_c A_m \cos 2\pi f_m t \cos^2 2\pi f_c t$
 $= \frac{A_c A_m}{2} \cos 2\pi f_m t [1 + \cos 2\pi (2f_c) t]$

where we use : $\cos^2 \alpha = \frac{1}{2} [1 + \cos 2\alpha]$

Now, taking the Fourier transform, we have :

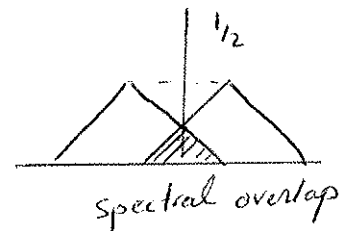


Drill 3.7



assuming that $f_c < w$

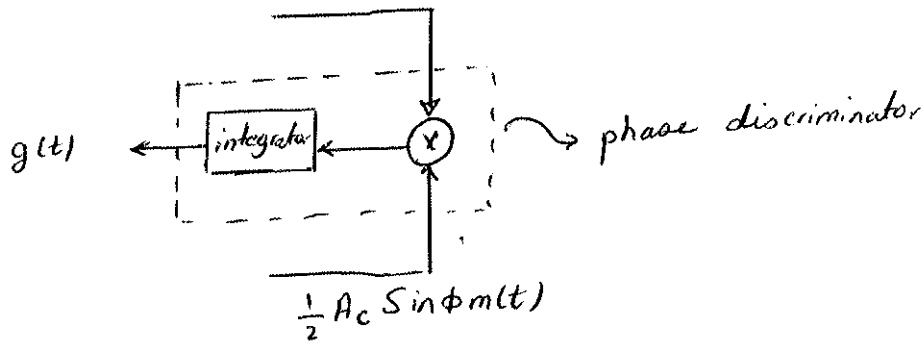
$F(m(t) \cos 2\pi f_c t)$ is \rightarrow



The effects of the spectral overlap can not be mitigated using a coherent detector.

Drill 3.8

$$\frac{1}{2} A_c \cos \phi m(t)$$



$$\Rightarrow g(t) = \frac{1}{2T} \int_{-T}^T \frac{1}{4} A_c^2 \cos \phi \sin \phi m^2(t) dt$$

$$= \frac{1}{4} A_c^2 \underbrace{\cos \phi \sin \phi}_{\frac{1}{2} \cos 2\phi} \cdot \frac{1}{2T} \int_{-T}^T m^2(t) dt \stackrel{(*)}{=} \frac{1}{4} A_c^2 \phi \cdot \frac{1}{2T} \int_{-T}^T m^2(t) dt$$

ϕ is small $\Rightarrow \cos 2\phi \approx 2\phi$ (*)

Now $2T \gg \frac{1}{W}$

$$\Rightarrow \frac{1}{2T} \int_{-T}^T m^2(t) dt = \frac{1}{W} m_p(t)$$

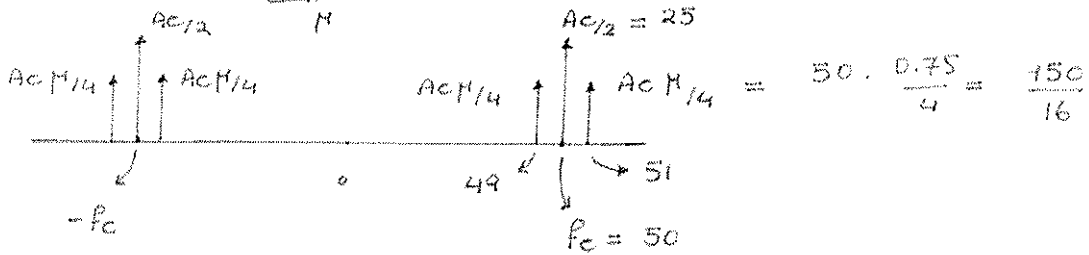
$$\Rightarrow g(t) = \frac{1}{4} A_c^2 \phi \cdot \frac{1}{W} \cdot m_p(t)$$

5. problem 3.18.

$m(t) = 20 \cos(2\pi t)$ message. (1 Hz)

$c(t) = 50 \cos(100\pi t)$ carrier (50 Hz) $A_c = 50$

AM $s(t) = A_c \left(1 + \underbrace{k_a A_m}_{M} \cos(2\pi t) \right) \cos(100\pi t)$.



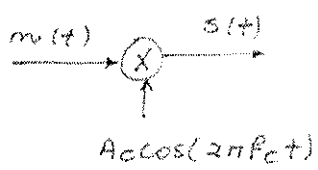
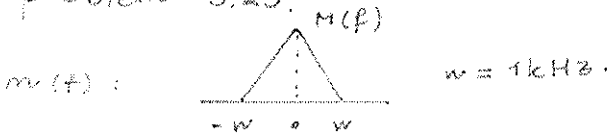
(a) $M = 0.75$ 75 percent modulation

(b) power across 100- Ω : $P = \frac{1}{100} (A_c/2)^2 + \frac{1}{100} (A_c^2 M^2 / 8 \times 2)$

$$= \frac{25 \times 100}{200} + \frac{25 \times 100 \times 0.75^2}{400}$$

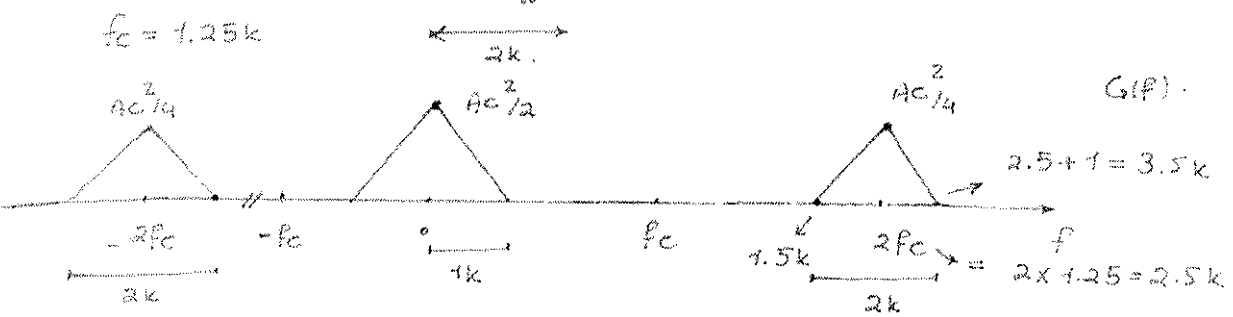
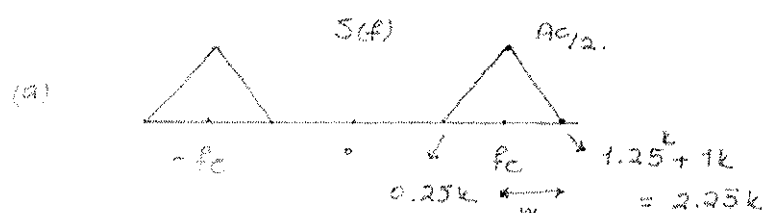
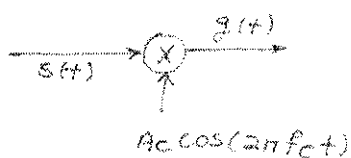
$$= 12.5 + 3.5156 = \underline{16.02}$$

6. problem 3.23.

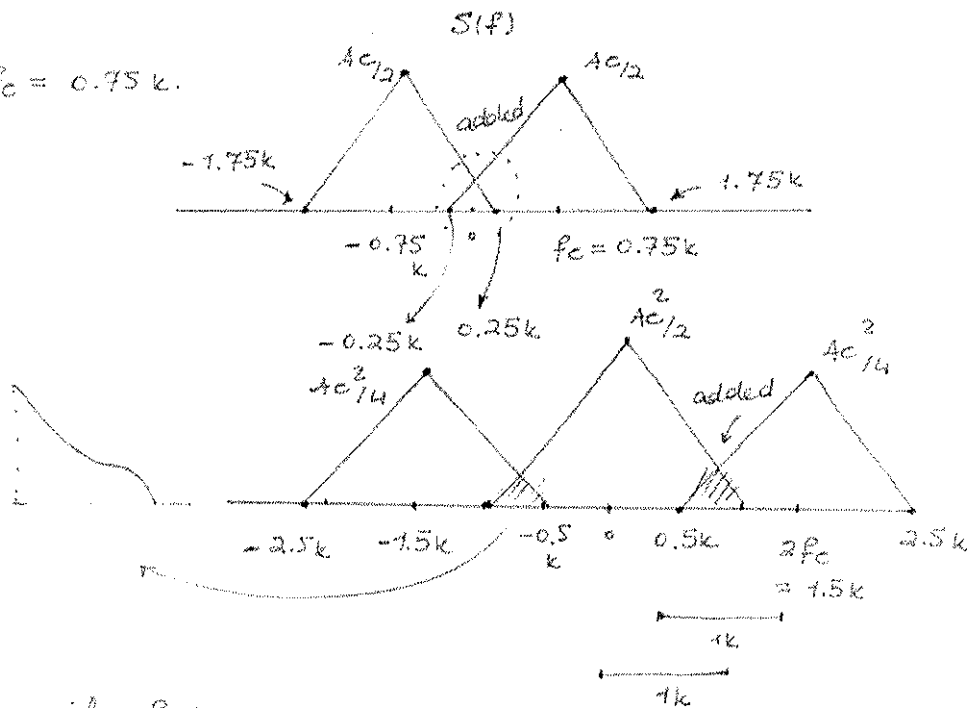


$A_c \cos(2\pi f_c t)$: carrier

Detector :



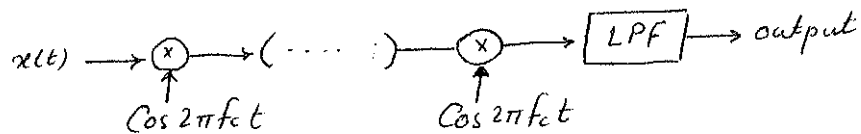
(b) if $f_c = 0.75k$.



Therefore: if $f_c > w$

- $\Rightarrow 2f_c > 2w \Rightarrow$ the high freq. component centered at $2f_c$ will not overlap with the base-band component.
- \Rightarrow Both components of the signal are uniquely determined. Hence $f_c > 1k Hz$

Problem 3.25. Coherent detector



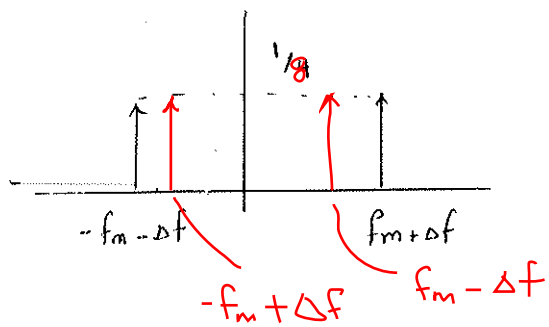
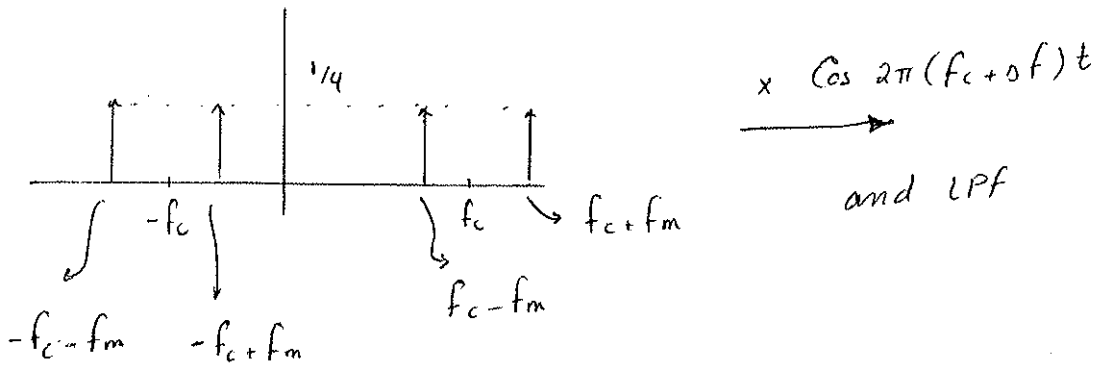
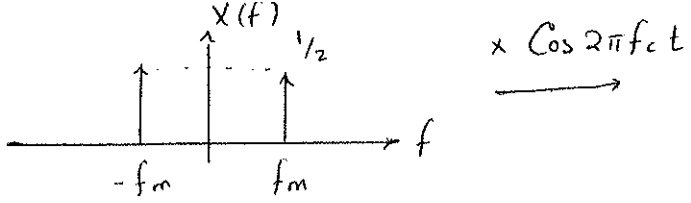
incoming DSB signal: $x(t) \cos 2\pi f_c t$

if there is an error $\Rightarrow \cos 2\pi(f_c + \Delta f)t$ at the receiver side.

$$\Rightarrow x(t) \cos 2\pi f_c t \cdot \cos 2\pi(f_c + \Delta f)t = \frac{1}{2} x(t) [\cos 2\pi \Delta f t + \cos 2\pi(2f_c + \Delta f)t]$$

Therefore, without any error, i.e., $\Delta f = 0$, the msg signal can be recovered using a LPF. However, with $\Delta f \neq 0$ (but Δf small), $\cos 2\pi \Delta f t$ appears as an extra term.

(b) if $x(t) = \cos 2\pi f_m t \stackrel{f}{\Rightarrow}$ The FT of the output is:



Drill 3.9

$$s(t) = A_c m_1(t) \cos 2\pi f_c t + A_c m_2(t) \sin 2\pi f_c t$$

Consider the upper branch.

$$x(t) = s(t) \cdot A_c' \cos 2\pi f_c t = A_c A_c' m_1(t) \cos^2 2\pi f_c t + A_c A_c' m_2(t) \cos 2\pi f_c t \times \sin 2\pi f_c t$$

$$= \frac{A_c A_c' m_1(t)}{2} + \frac{1}{2} A_c A_c' \cos 2\pi(2f_c)t + \frac{1}{2} A_c A_c' m_2(t) \sin 2\pi(2f_c)t$$

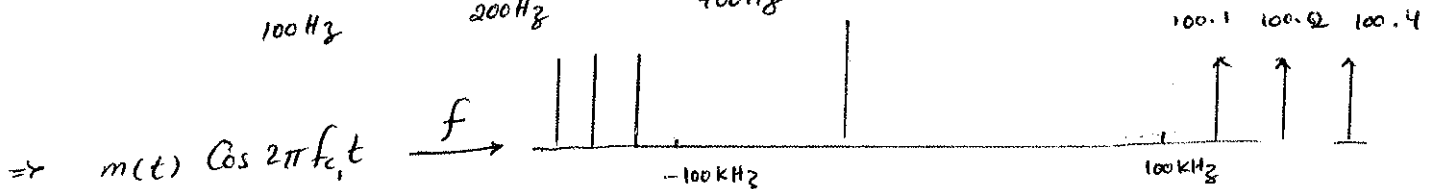
↓ high freq. high freq.

⇒ output of the LPF is $\frac{A_c A_c'}{2} m_1(t)$.

In a similar way, the output of the lower branch can be derived.

3.27.

$$m(t) = \underbrace{\cos 2\pi f_1 t}_{100\text{Hz}} + \underbrace{\cos 2\pi f_2 t}_{200\text{Hz}} + \underbrace{\cos 2\pi f_3 t}_{400\text{Hz}}$$

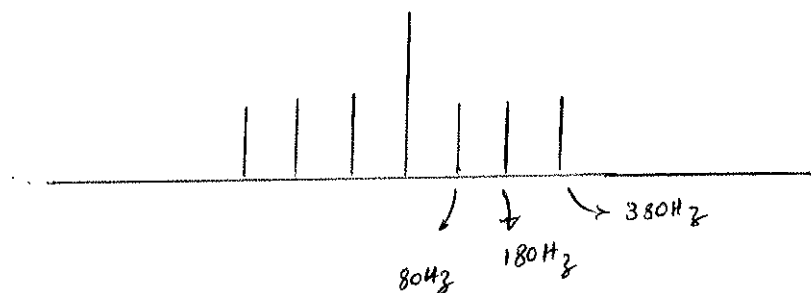


$$f_c = 100 \text{ kHz}$$

⇒ At the receiver side:

$$x \cos 2\pi f_c t$$

$$f_c = 100.02 \text{ kHz}$$

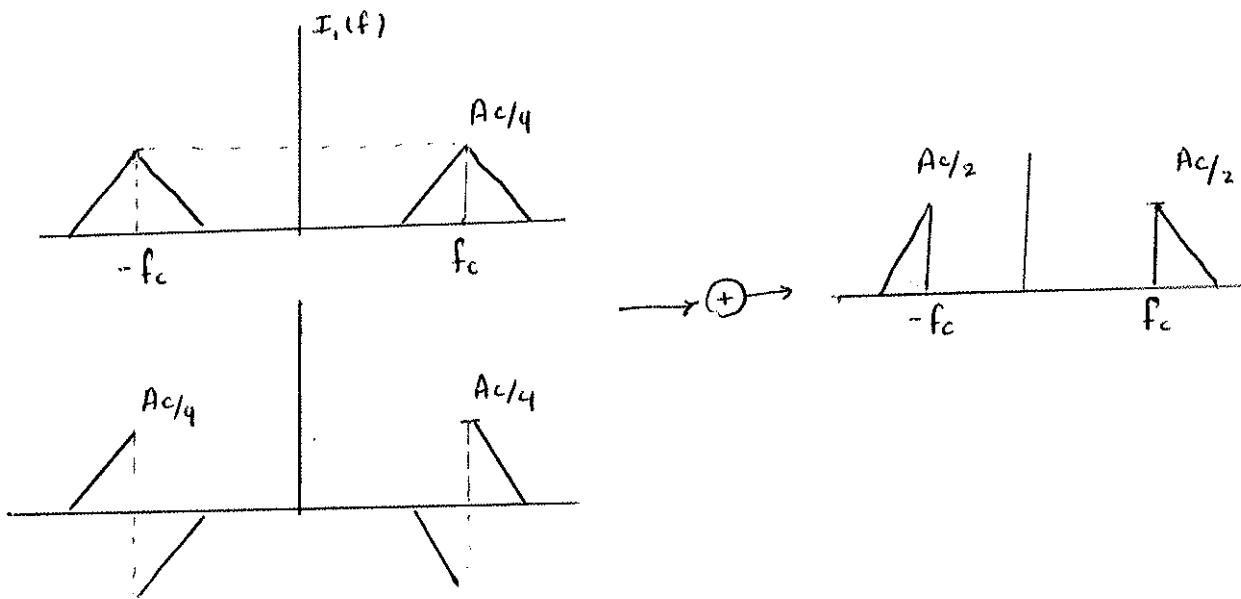


Drill 3.10.

$$s(t) = \frac{A_c}{2} m(t) \cos 2\pi f_c t - \frac{A_c}{2} \hat{m}(t) \sin 2\pi f_c t$$

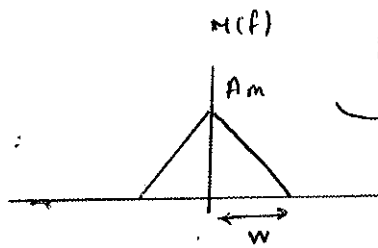
$$\hat{m}(t) \xrightarrow{F} -j \text{Sgn}(f) M(f)$$

$$\Rightarrow s(f) = \underbrace{\frac{A_c}{4} M(f) * [\delta(f-f_c) + \delta(f+f_c)]}_{I_1(f)} - \underbrace{\frac{A_c}{4} (-j \text{Sgn}(f) M(f)) \cdot \frac{1}{2j} (\delta(f-f_c) - \delta(f+f_c))}_{I_2(f)}$$

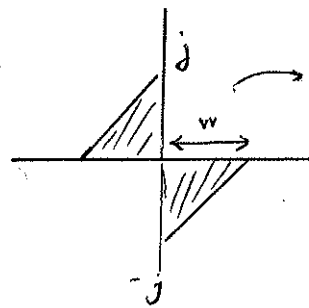


Drill 3.11

Suppose that:



Hilbert



still it is lowpass and $BW = w$

Drill 3.12.

Same as Drill. 3.7

Drill 3.13.

$$s(t) = \frac{A_c}{2} m(t) \cos 2\pi f_c t - \frac{A_c}{2} \hat{m}(t) \sin 2\pi f_c t \longrightarrow \text{Coherent detector} \\ \times A_c' \cos 2\pi f_c t$$

$$s(t) \times A_c' \cos 2\pi f_c t = \frac{A_c A_c'}{2} m(t) \cos^2 2\pi f_c t - \frac{A_c A_c'}{2} \hat{m}(t) \underbrace{\cos 2\pi f_c t \sin 2\pi f_c t}_{\text{high freq.}}$$
$$= \frac{A_c A_c'}{4} m(t) [1 + \underbrace{\cos 2\pi(2f_c)t}_{\text{high freq.}}]$$

\Rightarrow Output of the LPF is

$$\frac{A_c A_c'}{4} m(t)$$

$$(11) \quad s(t) = A_c m_1(t) \cos 2\pi f_c t + A_c m_2(t) \sin 2\pi f_c t$$

$$\rightarrow g_1(t) \text{ before LPF} = A_c m_1(t) \cos 2\pi f_c t \cos(2\pi f_c t + \phi) + A_c m_2(t) \sin 2\pi f_c t \cos(2\pi f_c t + \phi)$$

$$= \frac{A_c m_1(t)}{2} \overset{\text{high freq.}}{\cos(4\pi f_c t + \phi)} + \frac{A_c m_1(t)}{2} \cos \phi$$

$$+ \frac{A_c m_2(t)}{2} \sin(4\pi f_c t + \phi) - \frac{A_c m_2(t)}{2} \sin \phi$$

\downarrow
 high freq.

$$\Rightarrow g_1(t) = \frac{A_c m_1(t)}{2} \cos \phi - \frac{A_c m_2(t)}{2} \sin \phi$$

$g_2(t)$ can be derived in a same way.

$$(12) \quad g(t) = \cos 2\pi f_c t \Rightarrow G(f) = \frac{1}{2} \delta(f - f_c) + \frac{1}{2} \delta(f + f_c)$$

$$\Rightarrow \hat{g}(t) : \hat{G}(f) = -j \operatorname{Sgn}(f) \cdot \left[\frac{1}{2} \delta(f - f_c) + \frac{1}{2} \delta(f + f_c) \right]$$

$$= -j/2 \delta(f - f_c) + j/2 \delta(f + f_c)$$

$$= \frac{1}{2j} \left[\delta(f - f_c) - \delta(f + f_c) \right]$$

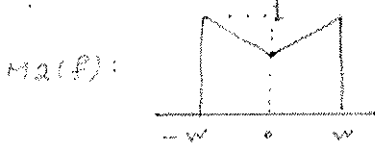
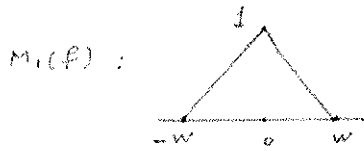
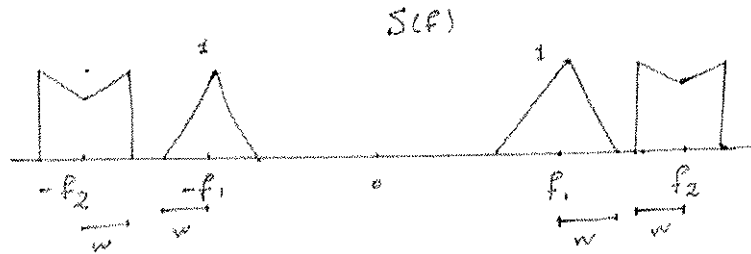
$$\underbrace{\hspace{10em}}_{\downarrow f^{-1}}$$

$$\sin 2\pi f_c t$$

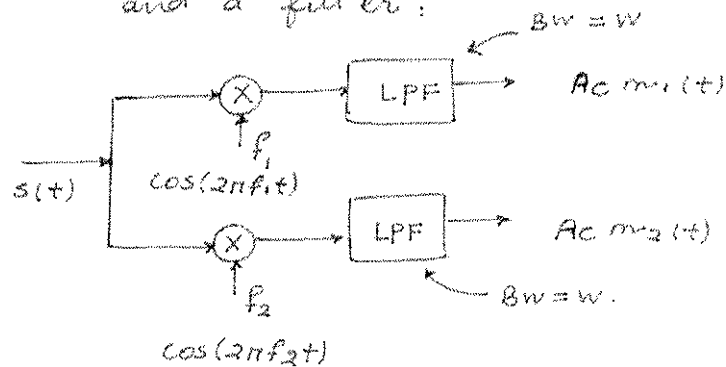
(13) Same as Drill 3.11.

6. $S(t) = A_c m_1(t) \cos(2\pi f_1 t) + A_c m_2(t) \cos(2\pi f_2 t)$

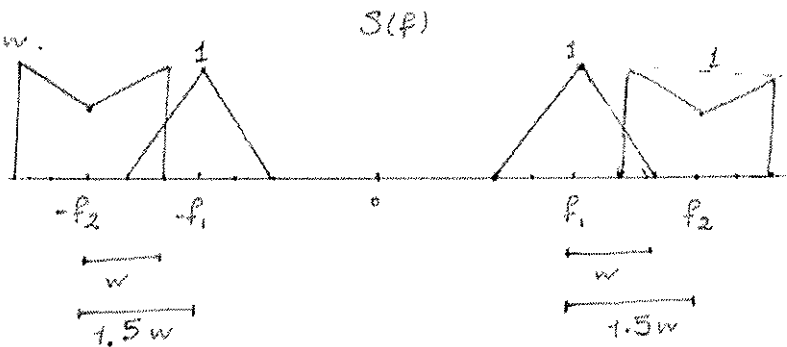
(a) $f_2 - f_1 > 2w$.



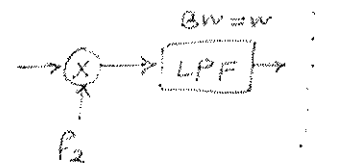
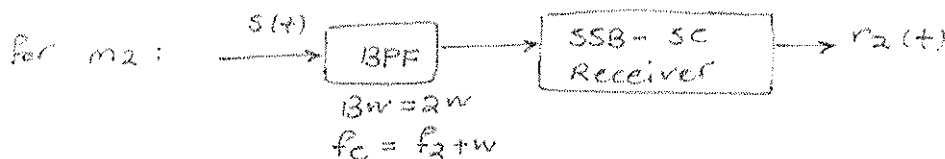
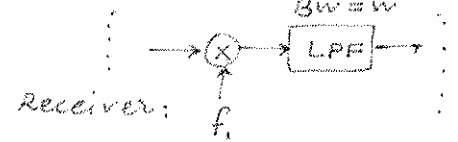
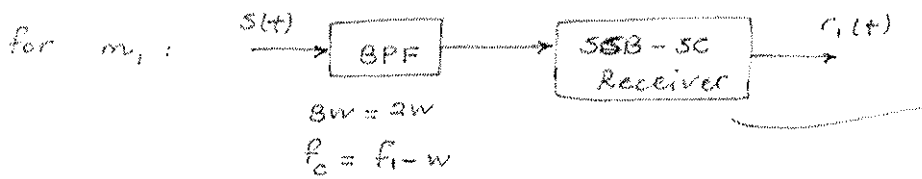
since $f_2 - f_1 > 2w \Rightarrow$ each signal can be recovered separately with a down-convert. and a filter:



(b) $f_2 - f_1 = 1.5w$.



Block Diagram for SSB-SC Receiver.



Supplement
Q2.

$$s(t) = A_c m_1(t) \cos(2\pi f_c t) + A_c m_2(t) \sin(2\pi f_c t)$$

$$s(t) \cos(2\pi f_c t + \phi)$$

$$= A_c m_1(t) \cos(2\pi f_c t) \cos(2\pi f_c t + \phi) + A_c m_2(t) \sin(2\pi f_c t)$$

$$\cos(2\pi f_c t + \phi)$$

$$= \frac{1}{2} A_c m_1(t) [\cos \phi + \cos(2\pi 2f_c t + \phi)] +$$

$$\frac{1}{2} A_c m_2(t) [\sin(2\pi 2f_c t + \phi) + \sin(-\phi)]$$

LPF

$$\rightarrow g_1(t) = \frac{1}{2} A_c m_1(t) \cos \phi + \frac{1}{2} A_c m_2(t) \sin(-\phi)$$

$$= \frac{1}{2} A_c [\cos \phi m_1(t) - \sin \phi m_2(t)]$$

$$s(t) \sin(2\pi f_c t + \phi)$$

$$= A_c m_1(t) \cos(2\pi f_c t) \sin(2\pi f_c t + \phi) + A_c m_2(t) \sin(2\pi f_c t)$$

$$\sin(2\pi f_c t + \phi)$$

$$= \frac{1}{2} A_c m_1(t) [\sin(2\pi f_c t + \phi) + \sin \phi] +$$

$$\frac{1}{2} A_c m_2(t) [\cos \phi - \cos(2\pi 2f_c t + \phi)]$$

LPF

$$\rightarrow g_2(t) = \frac{1}{2} A_c [\sin \phi m_1(t) + \cos \phi m_2(t)]$$